

喷片孔径及施药压力对果园喷雾机械 雾滴粒径和沉积分布的影响

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摘要:【目的】探究果园主要喷雾机械雾滴粒径及压力与农药冠层分布的关联, 为果园主要喷雾机械的设计、果农对喷雾机械的选择和使用提供技术参考。【方法】选取目前果园最常用的担架柱塞泵式机动喷雾机和自走传统轴流风送喷雾机为研究对象, 分析了两种喷雾机械在不同孔径、压力下的雾滴粒径, 并测试了雾滴在果园中的冠层沉积分布参数, 同时比较了两种喷雾机械的地面流失率与有效沉积率。【结果】1) 两种喷雾机械喷出的雾滴粒径均随孔径的减小和压力的增大而减小。当压力增至 2 MPa 时, 担架柱塞泵式机动喷雾机喷出的雾滴粒径受压力的影响明显减小。2) 两种喷雾机械的雾滴沉积分布, 均为冠层外侧沉积高于内侧, 其中担架柱塞泵式机动喷雾机的冠层中部雾滴沉积量最高, 下部次之, 顶部最低。区别于担架柱塞泵式机动喷雾机, 自走传统轴流风送喷雾机雾滴沉积量最高的区域为冠层下部, 中部次之。3) 两种喷雾机械喷孔直径减小, 降低雾滴粒径, 提高有效沉积率, 并降低地面流失率, 但自走传统轴流风送喷雾机中雾滴粒径的减小对地面流失率的影响有限。4) 在乔化稀植果园中, 担架柱塞泵式机动喷雾机, 孔径为 0.7 mm 时地面流失率最小, 为 22.04%, 有效沉积率最大, 为 45.92%。自走传统轴流风送喷雾机, 当孔径为 0.5 mm 时有效沉积率最大, 为 35.30%。【结论】两种喷雾机械在冠层上的流失途径不同, 担架柱塞泵式机动喷雾机的冠层流失源于所喷药液在叶片的沉积量超过叶片最大持留量, 进而导致药液滚落。而自走传统轴流风送喷雾机的冠层流失源于缺少变量喷雾技术而导致无效喷药量的产生。基于两种喷雾机械的流失特点进行针对性改进, 可以大幅提高其有效沉积率, 减少农药的施用量。

关键词:果园; 喷雾机械; 粒径; 冠层沉积分布; 地面流失率; 有效沉积率

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Influence of nozzle pore diameter and spraying pressure on size and deposition distribution of droplets from two types of orchard spray machines

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Abstract:【Objective】Chemical pesticide plays an irreplaceable role in control of plant diseases, pests and parasitic weeds and guarantees food security. Rational use of pesticide is helpful for improving agricultural productivity and crop quality. The pesticide spraying is still the main control method for pest control. Thus, the machine used for plant protection is important in orchards. At present, the machine presents a new situation, which is the motorized spray gun with high-capacity and high-pressure is the main stream and the air-blast spray with low-capacity is auxiliary. Compared with developed countries, the machine used for plant protection is relatively backward in China. However, the basic research is comparable with developed countries in China. The research is not in touch with the practical applica-

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tion. It is necessary to carry out basic and practical research on the machine used for plant protection in orchards. 【Methods】In this paper, the volume median diameters (VMD) of two common spray machines in orchards (motorized sprayer with stretcher and plunger pump and conventional axial flow sprayer) under different pressures and pore sizes were studied. The droplet deposition distribution, ground loss rate and effective deposition amount of two machines applied on the apple trees were measured. The relationship of droplet size and pressure of machines and canopy distribution of pesticide in orchards was studied and parameters were optimized. It can provide technical guidance for the design and choice of spraying machinery in orchards. 【Results】The research showed that the VMD of droplet decreased with the increase of pressure for motorized sprayer with stretcher and plunger pump at three pore sizes (0.7 mm, 1.0 mm and 1.4 mm). However, the decrease of VMD tended to be stable with the continuous increase of pressure. When the pressure was greater than 2 MPa, the effect of distance and pressure on particle size of the droplets reduced greatly. When the pressures were 1.5-3.5 MPa, the distribution ranges of particle size were from 180 μm to 250 μm for motorized sprayer with stretcher and plunger pump and conventional axial flow sprayer. In addition, the change of droplet size of conventional axial flow sprayer with spraying distance was larger than that of motorized sprayer with stretcher and plunger pump. For motorized sprayer with stretcher and plunger pump, the deposition in the middle of fruit tree canopy was the highest, followed by the lower part of fruit tree canopy, and the deposition in the upper part was lowest. The deposition of fruit tree canopy increased with the increase of pore size for motorized sprayer with stretcher and plunger pump at three pore sizes of 0.7 mm, 1.0 mm and 1.4 mm. With the pore size of 1.4 mm, the depositions in the middle and outer part of fruit tree canopy were the largest ($29.48 \text{ m} \cdot \text{m}^{-2}$). With the pore size of 0.7 mm, the depositions in the top and inner part of fruit tree canopy were the smallest ($5.14 \text{ m} \cdot \text{m}^{-2}$). By comparing to the ground loss rate and the effective deposition rate, it could be seen that the ground loss rate of motorized sprayer with stretcher and plunger pump increased with the increase of pore size, while the effective deposition rate decreased with the increase of pore size, which had an obviously negative correlation. When the pore size was 0.7 mm, the ground loss rate was the lowest (22.04%) and the effective deposition rate was the highest (45.92%). When the pore size was 1.4 mm, the ground loss rate was the largest (35.21%) and the effective deposition rate was the smallest (35.87%). There was a slight difference in the deposition structure of canopy after spraying between conventional axial flow sprayer and motorized sprayer with stretcher and plunger pump. The area with the most deposition was the lower part of the canopy, followed by the middle part, and the upper part was least. Compared with motorized sprayer with stretcher and plunger pump, under the condition of small pore size (0.5 mm), the amounts of deposition in and out of the upper canopy were similar, ranging from $5.49 \text{ m} \cdot \text{m}^{-2}$ to $6.66 \text{ m} \cdot \text{m}^{-2}$. However, under the condition of other pore sizes (0.7 mm and 1.0 mm) and canopy area (middle and lower), the amount of deposition of conventional axial flow sprayer was far lower than that of motorized sprayer with stretcher and plunger pump. It could be seen that the ground losses of the conventional axial flow sprayer at three pore sizes were not significantly different, ranging from 16.34% to 17.78%, which were far lower than that of motorized sprayer with stretcher and plunger pump. It could be seen that the effective deposition rate of the conventional axial flow sprayer increased with the decrease of the pore size. When the pore size was 0.5 mm, the effective deposition rate reached the highest by 35.30%, which was equivalent to the effective deposition rate of the motorized sprayer with stretcher and plunger pump at 1.4 mm pore size. 【Conclusion】For the motorized sprayer with stretcher and plunger pump, reducing the diameter of nozzle hole could decrease the droplet size, which was helpful to improve the effective deposition rate and reduce the ground loss rate. For the conventional axial flow sprayer, although reducing the droplet size had a

certain effect on improving the effective deposition rate, the effect on the ground loss rate was limited. There was difference in the route of liquid loss between two machines. The loss route of the conventional axial flow sprayer was mainly by means of the amount of droplet floating in the air. However, the loss route of the motorized sprayer with stretcher and plunger pump was mainly caused by the liquid falling from the leaf surface. In order to improve the effective deposition rate of two machines, the author proposed the corresponding improvement measures, such as adding air feeding device on the motorized sprayer with stretcher and plunger pump, or installing infrared detector on the conventional axial flow sprayer to realize variable spraying.

Key word: Orchard; Spray machine; Particle size; Deposition distribution of canopy; Ground loss rate; Effective deposition rate

目前化学农药在防治病虫草害和保证国家粮食安全方面依然发挥着不可替代的作用,合理使用农药有助于提高农业生产力和农作物质量。对于果园病虫害的防治,喷施农药依然是主要防治手段,据统计目前果园每年喷施农药8~15次^[1],其工作量约占果树管理工作总量的30%^[2-3],因此果园植保机械尤为重要。我国果园多为传统的乔砧密植型,当前植保机械仍以机动高压喷枪(即担架柱塞泵式机动喷雾机)为主^[4]。近些年随着农村劳动力人口的短缺,以及标准化矮砧密植型果园的出现,各种果园风送式喷雾机等新型植保机械逐渐出现在果园植保防控中^[5]。然而,我国传统果区依然存在大量密闭型老式果园,空间格局导致大型风送式果园喷雾机使用受限^[6]。目前我国果园植保防控呈现大容量机动高压喷枪喷雾为主,风送式喷雾机中低容量喷雾为辅,多种植保机械并用的新局面。

与发达国家相比,我国果园植保机械整体较为落后,农药利用率偏低,仅为20%~40%,较发达国家低15%~25%^[7-8]。但我国在果园机械的基础研究方面与发达国家相当,主要集中在获取低容量喷雾技术/精确喷雾技术的风送式喷雾机上^[9-14]。研究与实际应用(尤其是老旧果区)严重脱节,因此,开展植保机械的果园应用基础研究非常必要。

农药雾滴经过植保机械喷施,沉积到作物靶标上,通过与靶标作用起到防治效果^[15]。在农药喷施中,液滴经过植保机械雾化部件雾化分散,从喷头喷出的呈现一定分布的雾滴直径通常称为雾滴粒径,单位为μm。雾滴粒径是衡量药液雾化程度和比较各类喷头雾化质量的重要指标。雾滴直径常用的表示方法有:体积中值中径(volume median diameter, VMD)、数量中值中径(number median diameter,

NMD)^[16]。如果雾滴群中细小雾滴数量较多,将使雾滴数量中径变小,但数量较多的细小雾滴总量在总施药液量中只占非常小的比例,因此数量中径不能正确地反映大部分药液的粒径范围^[17]。因此,笔者研究了两种最常用的果园喷雾机械(担架柱塞泵式机动喷雾机与自走传统轴流风送喷雾机)在不同压力、不同孔径下的体积中值中径(VMD),并测定了两种植保机械在苹果树冠层的雾滴沉积分布、地面流失率及有效沉积量。通过分析两种植保机械的优缺点,进而优化使用参数,提高传统植保机械在果园中的农药有效利用率。

1 材料和方法

1.1 试验地点

试验在山西省晋中市开展,果树品种为富士,树龄20 a(年),栽种模式为乔化稀植型(间伐改造果园)。树高5.0~5.5 m,株距5.0 m,喷雾时温度25 °C,相对湿度65%。试验时间为2020年6月。

1.2 试验药剂

食品染色剂诱惑红(上海笛柏生物科技有限公司)。

1.3 试验仪器设备

雾滴激光粒度仪(济南微纳),担架柱塞泵式机动喷雾机[3WZ-25物理农林机械科技(苏州)有限公司,配套高压软管长为六胶八线管,长30 m内径8.5 mm×14 mm,工作压力10 MPa,爆破压力20 MPa](表1、图1),自走传统轴流风送喷雾机(3WG-8江苏南通广益机电有限公司)(表1、图2),多功能酶标仪(Synergy HTX美国伯腾仪器有限公司),LAI-2000植物冠层扫描仪(美国LI-COR Biosciences公司),流量计[LZT-15(1~11 L·min⁻¹)余姚远大]。

表1 两种机型主要参数

Table 1 Main parameters of the two models of sprayers

参数 Parameter	担架柱塞泵式机动喷雾机 Motorized sprayer of stretcher and plunger pump (3WZ-25)	自走传统轴流风送喷雾机 Conventional Axial flow sprayer (3WG-8)
配套功率 Supporting power/kW	6.6	6.6
喷头数量 Number of nozzles	1	8
最大/工作压力 Max/Working pressure/MPa	5	1-3
喷药量 Dosage of pesticide/(L·h ⁻¹)	450-930	200-800
水平喷幅 The level of sprinkling width/m	-	8-12
垂直射程 Vertical rang/m	3-10(自测 Self-determined)	4-6
风机形式 Fan form	-	轴流式 Axial flow
行走速度 Speed of travel/(km·h ⁻¹)	-	1.5-4.0



图1 担架柱塞泵式机动喷雾机

Fig. 1 Motorized sprayer of stretcher and plunger pump



图2 自走传统轴流风送喷雾机

Fig. 2 Conventional Axial flow sprayer

1.4 试验方法

1.4.1 粒径分布测定 利用雾滴激光粒度仪对担架柱塞泵式机动喷雾机和自走传统轴流风送喷雾机在不同孔径、压力下产生的雾滴粒径分布进行测定。其中,体积中值中径(VMD)为一次喷雾中,将全部

雾滴的体积从小到大顺序累加,当累加值等于全部雾滴体积的50%时,所对应的雾滴直径。

1.4.2 雾滴在果树冠层和地面的沉积量测定 采用担架柱塞泵式机动喷雾机和自走传统轴流风送喷雾机,以同列4株树为1个试验小区,选取6列为试验对象,其中担架柱塞泵式机动喷雾机对每小区果树进行逐一喷施诱惑红药液($550 \text{ mg} \cdot \text{L}^{-1}$),并在喷施前后称取药箱药液质量,以前、后药液质量差为施药量。轴流风送果园喷雾机在树冠两侧以固定的行进速度喷施诱惑红药液($550 \text{ mg} \cdot \text{L}^{-1}$),在喷雾机出药管道输出处安装流量计,记录喷药时间,计算总喷药量。并在树干两侧由内向外布设 $23 \text{ cm} \times 15 \text{ cm}$ 的塑料布,按照距离树干位置布置10个取样点,每个取样点相距50 cm,每个样点重复3次,用于采集地面流失药液(图3)。同时在树冠上按东西南北,上中下三层,每层分内膛和外膛,共24个取样点,将收集、采集回来的塑料布和叶片,分别置于塑封带中带回实验室,加入50 mL清水,振荡洗涤10 min,用多

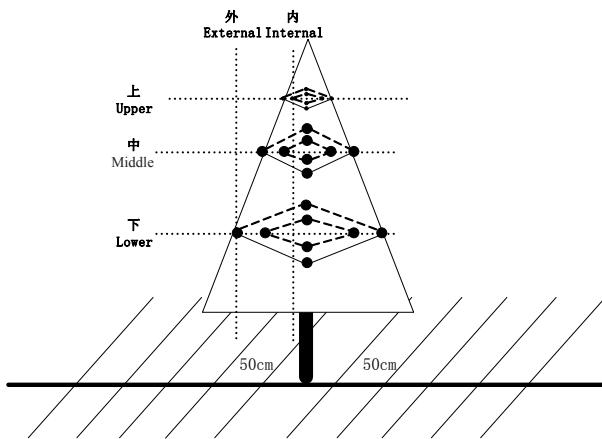


图3 苹果园测定叶片沉积分布与地面流失量采样示意图

Fig. 3 Schematic diagram of measurement of deposition distribution and ground loss amount in apple orchard

功能酶标仪测定洗涤液的诱惑红浓度,波长选择501 nm,苹果叶片利用扫描仪和ImageJ软件测定面积。计算果树冠层不同部位的沉积量(图3)。

1.4.3 冠层地面投影面积测定 假设所要测量的小区内4株树为同一冠层,选取小区列最外侧距离为长,单株最外侧距离为宽,圈定一矩形为冠层阴影面积。

1.4.4 叶面积指数的测定 指单位土地面积上植物叶片总面积占土地面积的倍数,于喷雾前采用鱼眼影像技术测量植被冠层结构参数。使用LAI-2200植物冠层扫描仪,选择仪器自带90冠遮盖帽,对冠层阴影区采取“1上4下”采样方式(1上指空中没有任何冠层阻拦的背景遮光值,4下指冠层阴影区域内随机选取4个点的遮光数值)。仪器自动计算其叶面积指数^[17-18]。3次重复,取平均值。

1.5 数据处理及计算方法

1.5.1 地面流失率计算 根据实验室测定的洗涤液中指示剂诱惑红的浓度、洗涤液的体积和取样面积,按公式(1)计算喷雾后指示剂诱惑红在地面不同部位的沉积量($\text{mg}\cdot\text{cm}^{-2}$)。根据地面沉积量与喷雾小区指示剂的喷洒量,按公式(2)计算喷雾药液的地面流失率(%)。

$$p_1 = \frac{c \times V \times 10}{S_1}; \quad (1)$$

$$\eta_1 = \frac{p_1 \times S_2}{m} \times 100\%. \quad (2)$$

式中: p_1 为地面沉积量, $\text{g}\cdot\text{m}^{-2}$; c 为洗涤液的诱惑红质量浓度, $\text{mg}\cdot\text{mL}^{-1}$; V 为体积, mL ; S_1 为取样面积, cm^2 ; η_1 为地面流失率,%; S_2 为小区面积, m^2 ; m 为小

区内诱惑红投放量,g。

1.5.2 有效沉积率计算 根据实验室测定的洗涤液中指示剂诱惑红的浓度、洗涤单位面积内的诱惑红体积,按公式(3)计算喷雾后指示剂诱惑红在果树冠层叶片上的平均沉积量($\mu\text{g}\cdot\text{cm}^{-2}$)。根据叶片上的平均沉积量与冠层的总叶面积,计算全树叶片上的沉积量,其中总叶面积按公式(4)计算,再结合喷雾小区指示剂的喷洒量,按公式(5)计算喷雾药液在叶片上的有效沉积率(%)。其中叶面积指数是总叶面积与冠层地面积的比值^[5]。

$$p_2 = \frac{c \times V \times 10}{S_3}; \quad (3)$$

$$S_4 = LS_5; \quad (4)$$

$$\eta_2 = \frac{p_2 \times S_4}{m} \times 100\%. \quad (5)$$

式中: p_2 为叶片沉积量, $\text{g}\cdot\text{m}^{-2}$; c 为洗涤液中诱惑红质量浓度, $\text{mg}\cdot\text{mL}^{-1}$; V 为洗涤单位面积内的诱惑红体积, mL ; S_3 为叶片面积, cm^2 ; S_4 为总叶面积, m^2 ; L 为叶面积指数; S_5 为冠层投影面积, m^2 ; η_2 为有效沉积率,%; m 为小区内诱惑红投放量,g。

2 结果与分析

2.1 担架柱塞泵式机动喷雾机的粒径分布

对不同孔径的担架柱塞泵式机动喷雾机在不同压力下的粒径分布进行了测定,图4为0.7 mm孔径担架柱塞泵式机动喷雾机在不同压力下的粒径分布,随着压力的增大,雾滴的体积中值中径(VMD)呈减小趋势。当柱塞泵压力范围为2.5~3.5 MPa、喷施距离为2和3 m时,两种条件下的雾滴粒径相差较

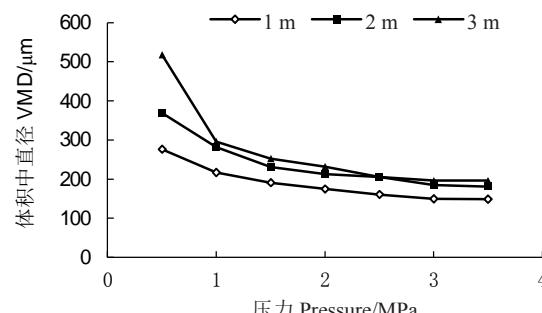


图4 0.7 mm孔径担架柱塞泵式机动喷雾机不同压力和喷施距离下的VMD

Fig. 4 VMD of motorized sprayer of stretcher and plunger pump with 0.7 mm stretcher plunger pump sprayer under different pressure and spraying distance

小,变化趋势相近;当喷施距离为1 m时,雾滴粒径最小,VMD为148.55 μm 。

图5为1.0 mm孔径担架柱塞泵式机动喷雾机在不同压力下的粒径分布,由图可知,雾滴粒径随着压力的增大和喷施距离的减小而减小,当柱塞泵压力为3.5 MPa、喷施距离为1 m时,雾滴粒径最小,VMD为168.13 μm ;喷施距离为2和3 m时,雾滴粒径相近,VMD分别为188.58和195.45 μm 。

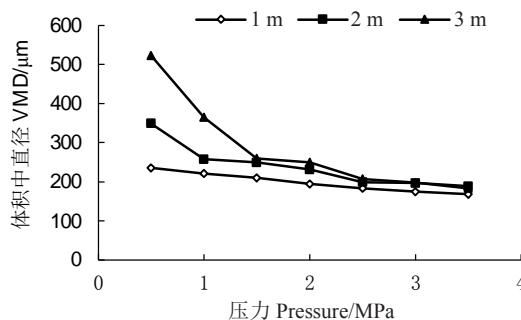


图5 1.0 mm孔径担架柱塞泵式机动喷雾机不同压力和喷施距离下的VMD

Fig. 5 VMD of motorized sprayer of stretcher and plunger pump with 1.0 mm under different pressure and spraying distance

图6为1.4 mm孔径担架柱塞泵式机动喷雾机在不同压力下的粒径分布,其变化趋势与0.7和1.0 mm所测结果相似,均是随着压力的增大及喷施距离的减小,雾滴粒径逐渐减小。除0.5 MPa外,柱塞泵1.0~3.5 MPa下1.4 mm孔径担架柱塞泵式机动喷雾机的雾滴粒径较0.7和1.0 mm均较大,说明在相同条件下,喷雾机械喷片孔径越大,雾滴粒径越

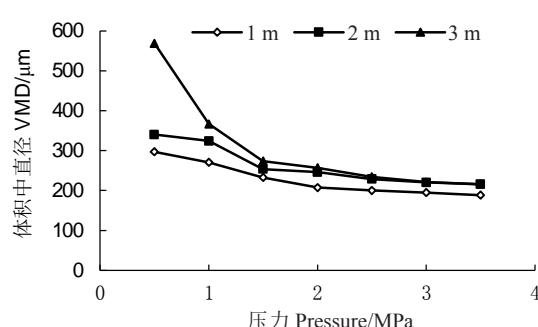


图6 1.4 mm孔径担架柱塞泵式机动喷雾机不同压力和喷施距离下的VMD

Fig. 6 VMD of motorized sprayer of stretcher and plunger pump with 1.4 mm under different pressure and spraying distance of 1.4 mm stretcher plunger pump sprayer under different pressure and spraying distance

大;此外,比较柱塞泵3.5 MPa下不同喷施距离的雾滴粒径可知,喷施距离为1 m的雾滴粒径最小,VMD为188.48 μm 。

通过上述三种孔径(0.7, 1.0, 1.4 mm)担架柱塞泵式机动喷雾机的测试分析可知,雾滴的VMD均随柱塞泵压力的增大而减小,这可能是因为,压力越大,液体流出喷孔的初速度就越大,喷孔中液体扰动程度及喷出后所受空气介质的阻尼也越大,雾滴更容易破碎。但随着压力的继续增大,VMD逐渐减小并趋于稳定(图7)。

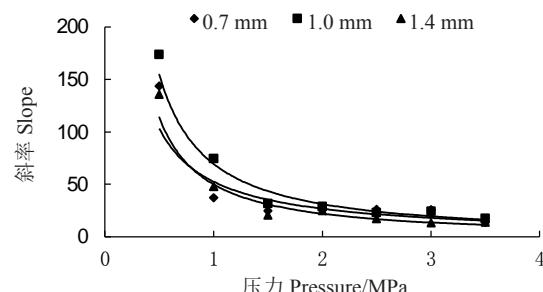


图7 不同喷孔下雾滴粒径随压力变化的斜率

Fig. 7 Slope of particle size of droplet with pressure under different pore size

从不同喷孔下的雾滴粒径随压力变化的斜率可以看出,雾滴粒径随着压力的增大,斜率逐渐减小,即压力越大,喷孔喷出的雾滴越稳定。当柱塞泵压力大于2 MPa时,喷出雾滴的粒径受距离和压力的影响大幅减弱。此外,雾滴粒径也随喷孔的减小而减小,原因可能源于喷孔直径越小,液体喷出喷孔时会受到更大的节流,喷孔内扰动增加,雾滴更易破碎。

2.2 自走传统轴流风送喷雾机的粒径分布

对不同孔径的自走传统轴流风送喷雾机在不同压力下的粒径分布进行了测定。基于压力低于1.5 MPa时,自走传统轴流风送喷雾机无法正常工作的实际情况,图8为1.5~3.5 MPa压力范围内的粒径分布。由图中可以看出,雾滴粒径均随压力的增加和孔径的减小而逐渐减小,当孔径为1.0 mm,压力为1.5 MPa时,雾滴粒径最大,为263.99 μm ;当孔径为0.5 mm,压力为3.5 MPa时,雾滴粒径最小,为197.02 μm 。

为了研究自走传统轴流风送喷雾机工作时气流输送对雾滴粒径造成的影响,重点测试了0.7 mm孔径自走传统轴流风送喷雾机在不同压力和喷施距离

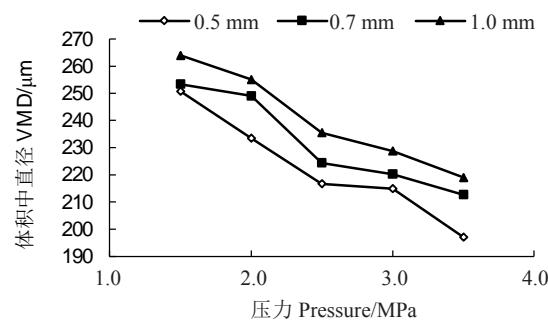


图 8 传统轴流风送喷雾机不同压力距喷孔

2 m 处的 VMD

Fig. 8 VMD of conventional axial flow sprayer under different pressure and 2 m from orifice

下雾滴的粒径分布,从图9可以看出,在同一喷施距离下,雾滴粒径随着压力的增大而减小;在同一压力下,雾滴粒径随着喷施距离的增大而增大。当压力为1.5 MPa、喷施距离为3 m时,雾滴粒径最大,为272.67 μm;当压力为3.5 MPa、喷施距离为1 m时,雾滴粒径最小,为201.09 μm。

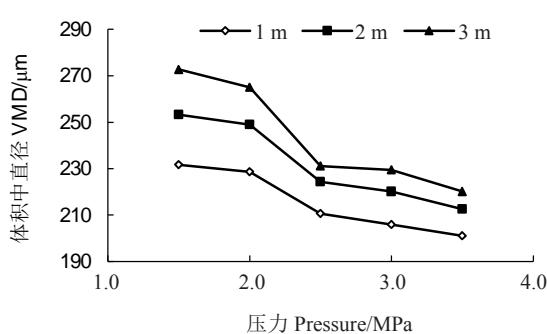


图 9 0.7 mm 孔径自走传统轴流风送喷雾机不同压力和喷施距离下的 VMD

Fig. 9 VMD of conventional axial flow sprayer with 0.7 mm under different pressure and spraying distance

由上述结果可知,担架柱塞泵式机动喷雾机与自走传统轴流风送喷雾机在压力为1.5~3.5 MPa时,粒径分布范围基本一致,在180~250 μm(表2)。但相同压力下,担架柱塞泵式机动喷雾机的雾滴粒径小于自走传统轴流风送喷雾机的雾滴粒径。此外,自走传统轴流风送喷雾机的雾滴粒径随喷施距离的

表 2 两种喷雾机械在不同压力下的粒径分布

Table 2 VMD under different pressure of two kinds of spraying machines

μm

处理 Treatment	喷片孔径 Pore size/mm	距喷口距离 Spraying distance/m	压力 Pressure/MPa						
			0.5	1.0	1.5	2.0	2.5	3.0	3.5
担架柱塞泵式喷雾机 Motorized sprayer of stretcher and plunger pump	1.4	1	297.43	270.78	232.95	207.42	200.63	195.02	188.48
		2	340.85	324.44	253.50	245.80	229.04	220.77	215.69
		3	568.66	366.56	273.78	256.78	234.65	221.05	215.99
	1.0	1	235.71	221.20	210.19	194.02	183.58	174.39	168.13
		2	349.37	257.67	249.36	231.86	199.15	196.86	188.58
		3	522.95	364.96	259.74	249.35	206.65	197.69	183.21
	0.7	1	275.61	216.59	189.86	174.72	160.42	149.16	148.55
		2	368.53	281.39	230.50	212.11	205.37	184.88	180.52
		3	517.45	295.74	252.25	231.79	205.19	195.82	195.45
自走传统轴流风送 喷雾机 Conventional Axial flow sprayer	0.5	2	—	—	250.79	233.44	216.68	214.94	197.02
	0.7	1	—	—	231.75	228.63	210.70	205.92	201.09
		2	—	—	253.33	249.06	224.35	220.18	212.59
		3	—	—	272.66	265.01	231.14	229.41	220.18
	1.0	2	—	—	263.99	255.07	235.47	228.77	219.03

变化大于担架柱塞泵式机动喷雾机。

2.3 担架柱塞泵式机动喷雾机与自走传统轴流风送喷雾机的沉积分布规律

为研究施药机械雾滴粒径分布对冠层沉积分布、地面流失率的影响,选取2.0 MPa压力下(机械推荐压力),对不同孔径下两种施药机械的果树冠层沉积分布和地面流失率进行了试验。结果见表3。

从表3可以看出,对于担架柱塞泵式机动喷雾

机,果树冠层中部的沉积量最高,下部次之,上部沉积量最低。0.7,1.0,1.4 mm三种孔径的担架柱塞泵式机动喷雾机在果树冠层的沉积量随喷雾孔径的增大而增大。其中果树冠层上部的沉积量随喷雾孔径增大的增长范围最大,内膛/外膛沉积量由5.14 g·m⁻²/7.49 g·m⁻²增大至22.14 g·m⁻²/24.94 g·m⁻²,可能原因为:担架柱塞泵式机动喷雾机的动力来源于液体压力,果树冠层上部距离喷口最远,孔径越大喷出的粒

表3 两种施药机械在果树冠层上的沉积分布和地面流失率

Table 3 The deposition distribution and ground loss rate of two kinds of spraying machines in the canopy of apple trees

处理 Treatment	孔径 Pore size/ mm	冠层 Canopy	沉积量 Deposition amount/(g·m ⁻²)		沉积比 Ratio/ (inner outer)	叶面积指数 Leaf area index	地面流失率 Ground loss rate/%	有效沉积率 Effective deposition rate/%
			内膛 Internal	外膛 External				
担架柱塞泵式 机动喷雾机 Motorized sprayer of stretcher and plunger pump	0.7	上 Upper	5.14	7.49	0.68	2.33	22.04	45.92
		中 Middle	23.23	28.35	0.82			
		下 Lower	22.33	23.16	0.96			
	1.0	上 Upper	15.14	20.68	0.73	30.04	40.56	
		中 Middle	25.91	29.81	0.87			
		下 Lower	21.92	22.17	0.99			
	1.4	上 Upper	22.14	24.94	0.89	35.21	35.87	
		中 Middle	27.48	29.48	0.93			
		下 Lower	24.09	26.09	0.92			
自走传统轴流风 送喷雾机 Conventional Axial flow sprayer	0.5	上 Upper	5.49	6.66	0.82	16.34	35.30	
		中 Middle	9.07	11.44	0.79			
		下 Lower	12.12	15.82	0.77			
	0.7	上 Upper	6.59	8.10	0.81	17.78	28.37	
		中 Middle	9.27	12.95	0.72			
		下 Lower	13.82	19.15	0.72			
	1.0	上 Upper	6.62	8.25	0.80	17.17	26.89	
		中 Middle	11.39	15.89	0.72			
		下 Lower	16.18	21.96	0.74			

径越大,液体通过大孔径所受节流小于小孔径,喷出雾滴携带能量较高,喷施距离较远。同时,孔径越大喷出药液量越大,以1.0 mm孔径为例,其单位时间内喷施药液量是0.7 mm孔径的1.8倍,上述因素共同导致同等压力下大孔径施药机械的果树冠层单位沉积量远高于小孔径施药机械。与冠层上部变化趋势不同,冠层中下部随施药机械孔径增大沉积量增长缓慢,其原因可能在于担架柱塞泵式机动喷雾机在果树冠层中部的沉积量均接近或超过叶片最大持留量,故表现出沉积量的相近性。对于担架柱塞泵式机动喷雾机,果树冠层沉积量最高的部位均集中于中部,主要原因在于中部区域高度几乎与施药人员上半身平齐,且为果树冠层最厚的区域,因此施药人员存在有意识过喷情况。通过比较果树冠层内外区域的沉积比可以看出,小孔径担架柱塞泵式机动喷雾机上部区域内外沉积比仅为0.68,随着喷雾孔径的增大和冠层部位的下降,内外沉积比不断提高,当喷雾孔径为1.0 mm时,在果树冠层下部区域和喷雾孔径为1.4 mm,在果树冠层中下部区域时,内外沉积比超过0.9。这在一定程度上证实了小孔径的雾滴喷射距离较短,从而导致冠层上部内外沉积比较低的结果。通过比较地面流失率与有效沉积率可

以看出,担架柱塞泵式机动喷雾机的地面流失率随喷雾孔径的增大而增大,有效沉积率随喷雾孔径的增大而减小,二者呈明显的负相关性。当喷雾孔径为0.7 mm时,地面流失率最小,为22.04%,有效沉积率最大,为45.92%。当喷雾孔径为1.4 mm时,地面流失率最大,为35.21%,有效沉积率最小,为35.87%。

自走传统轴流风送喷雾机施药后的冠层沉积结构与担架柱塞泵式机动喷雾机稍有差别,沉积量最多的区域为冠层下部,中部次之,上部最低。与担架柱塞泵式机动喷雾机相比,在小孔径条件下(0.5 mm),果树冠层上部的内外沉积量相似,为5.49~6.66 g·m⁻²。而在其他孔径(0.7, 1.0 mm)和冠层区域(中部, 下部)条件下,自走传统轴流风送喷雾机的叶面沉积量均远远低于担架柱塞泵式机动喷雾机。就内外膛沉积分布而言,自走传统轴流风送喷雾机的果树冠层内外分布与担架柱塞泵式机动喷雾机相似,均是内膛低于外膛,其中果树冠层上部的内外膛比值最高,三种孔径下的内外膛比值均在0.8以上,且没有显著差异。与担架柱塞泵式机动喷雾机相比,除0.5、0.7 mm孔径时冠层上部内外沉积较大外,其他条件下自走传统轴流风送喷雾机的内外膛比值均

低于担架柱塞泵式机动喷雾机。从地面流失率可看出,自走传统轴流风送喷雾机在三种孔径下的地面流失量相差不大,为16.34%~17.78%,均远低于担架柱塞泵式机动喷雾机。从有效沉积率可看出,自走传统轴流风送喷雾机的有效沉积率随喷雾孔径的减小而提高,当喷雾孔径为0.5 mm时,有效沉积率最高,为35.30%,与担架柱塞泵式机动喷雾机在喷雾孔径1.4 mm时的有效沉积率相当。通过分析有效沉积率可发现,对于担架柱塞泵式机动喷雾机,减小喷孔直径可导致雾滴粒径降低,确实有助于提高有效沉积率,并降低地面流失率。而对于自走传统轴流风送喷雾机,虽降低雾滴粒径对提高有效沉积率有一定效果,但对地面流失率的影响有限。

需要说明的是,此次对担架柱塞泵式机动喷雾机的试验,测量的工作压力是柱塞泵出水口的压力,考虑到机动喷雾机一般工作时都会连接较长的高压软管以输送药液,药液在高压软管中会有较大衰减。因此在试验结束后又对担架柱塞泵式机动喷雾机的出口压力进行了测试。测试结果见表4。

表4 担架柱塞泵喷雾机压力衰减对照表

Table 4 Pressure attenuation comparison of motorized sprayer of stretcher and plunger pump

处理 Treatment	压力 Pressure/MPa						
柱塞泵 Plunger pump	0.5	1.0	1.5	2.0	2.5	3.0	3.5
喷枪出口 Spray gun exports	0.3	0.5	0.8	1.0	1.3	1.5	1.8

由表4可以看出,经过高压软管的对药液的运输,阻塞泵压力的损失在50%~60%。但是对于担架柱塞泵喷雾机,机械推荐压力一般为柱塞泵出口压力,因此在实际操作过程中为保证喷雾质量,不能忽视输药管对压力的影响。

3 讨 论

通过上述研究发现,压力提高和喷片孔径减小,确实能降低雾滴粒径,但雾滴粒径并非无限减小。如对于担架柱塞泵式机动喷雾机,当压力大于2 MPa时,雾滴粒径受喷施距离、压力的影响均在大幅减弱。就果树冠层的沉积分布角度而言,雾滴粒径的减小确实可以提高农药的有效沉积率,这是因为小粒径雾滴自身质量轻,所携带能量也较少,当接触到植物靶标界面时,不易弹跳、滚落,小粒径雾滴更易覆着于叶片上^[19],从而提高了有效沉积率。此外,小粒径雾滴受空气阻力影响,动能衰减较快,雾

滴在沉降前漂移,增加了雾滴的漂移率,同时也降低了地面流失率^[20,21]。而对于自走传统轴流风送喷雾机,增强的辅助气流胁迫小粒径雾滴进入冠层内部,增加雾滴在冠层的穿透性,并且扭转叶片,使得叶片近、远轴面着药,故内外膛沉积比均能达到0.7~0.8以上。从果树冠层内外沉积比和有效沉积率来看,自走传统轴流风送喷雾机的内外沉积比低于担架柱塞泵式机动喷雾机,原因在于,担架柱塞泵式机动喷雾机对操作人员的要求较高,喷施人员可以自主在果树冠层内外施药,因此可以提高果树冠层内外沉积的比值。

比较两种施药机械的有效沉积率和地面流失率可以看出,担架柱塞泵式机动喷雾机的有效沉积率高于自走传统轴流风送喷雾机,这是由于此次试验果园为乔化稀植型,两树之间有较大空隙,故自走传统轴流风送喷雾机存在大量无效喷药量,且在果树冠层顶部雾滴飘移严重^[22]。但自走传统轴流风送喷雾机的地面流失率低于担架柱塞泵式机动喷雾机,其原因在于自走传统轴流风送喷雾机喷出的雾滴受辅助气流影响,飘散距离远大于担架柱塞泵式机动喷雾机,进而导致相应的地面流失率远低于担架柱塞泵式机动喷雾机。同时,结合担架柱塞泵式机动喷雾机的叶面沉积量与地面沉积率可以看出,担架柱塞泵式机动喷雾机的药液沉积量远高于自走传统轴流风送喷雾机,初步推断,担架柱塞泵式机动喷雾机药液量流失的主要原因在于,叶片上的药液量超过最大持留量,进而导致药液滴落流失。在笔者试验过程中,使用担架柱塞泵式机动喷雾机喷药后,在冠层地面阴影区域可收集到大量流失药液,也证实了以上推断。因此可得出,两种施药机械的药液流失途径有较大差别,自走传统轴流风送喷雾机的流失途径主要是雾滴在空中的漂移量,而担架柱塞泵式机动喷雾机的流失途径主要是药液的滚落。

针对两种施药机械不同的药液流失途径,笔者认为可采取相应的改进措施以提高其有效沉积率,对于担架柱塞泵式机动喷雾机,由现场试验可知,在2.0 MPa喷雾压力下,1.0 mm孔径时的沉积效果最佳,同时结合雾滴粒径可以得出,当雾滴VMD大于190 μm时(距离喷口1 m),雾滴在冠层上、中、下部位内外膛沉积在70%以上,当低于次粒径时,雾滴携带能量过低,到达果树冠层上部的雾滴有限,导致药液在冠层中部区域过多沉积并流失到地面,造成药

液浪费。但随着VMD增大,雾滴所携带能量也越大,导致液滴接触到叶片后所造成的弹跳流量失也会大幅提高。因此为提高担架柱塞泵式机动喷雾机的有效沉积率,应在降低雾滴沉积率的同时提高液滴的初始速度为其添加辅助气流。如采用0.7 mm孔径时在喷头处增设风送装置,提高雾滴初始速度,进而提高有效沉积率,同时还可适当降低机械压力延长部件使用寿命。此方法适用于间伐后的大型乔化果园春季清园或果园面积较小冠层密度较低的果园。对于自走传统轴流风送喷雾机,由于有辅助气流的帮助,即使喷口距离靶标叶片远,液滴依然可以随辅助气流飘入冠层中。因此从沉积结构来看,雾滴粒径(VMD:233.44~255.07 μm)的大小对冠层内外沉积比影响较小。而从冠层垂直分布上来看,冠层上部沉积量并未随雾滴的增大或压强的增大而明显提高,说明使用的该型号传统轴流风送喷雾机导流风向或送风量需要进行改进。同时由于变量喷雾技术的欠缺,导致在乔化稀植果园中的大量无效喷药。但当自走传统轴流风送喷雾机应用于矮砧密植果园时,其有效沉积率会大幅提高,如张鹏九等人对传统风送式喷雾机在不同栽种模式下果园的农药有效利用率进行了试验,结果表明,在相同条件下传统风送式喷雾机在矮砧密植果园的有效沉积率比稀植果园高出10%以上^[5,23]。而对于乔化稀植果园,自走传统轴流风送喷雾机应进行合理改进,如加装红外探测器,使其根据靶标作物的种植特点进行变量喷雾,即冠层密时喷雾量大,冠层稀时喷雾量小甚至不喷雾^[24-25],这样农药有效沉积率仍有很大提升空间。

同时,与目前果园新型植保器械无人机相比,虽然植保无人机防治效果有待进一步探索^[26],但由于喷药方向的差异导致传统植保机械与植保无人机的沉积结构有很强的互补性,植保无人机的沉积结构一般为冠层上部最大,中部次之,下部最低^[27-28]。因此植保无人机可以对传统果园植保机械进行一定的补充。

4 结 论

通过上述研究发现,压力提高和喷片孔径减小,确实能降低雾滴粒径,但雾滴粒径并非无限减小。如对于担架柱塞泵式机动喷雾机,当压力大于2 MPa时,雾滴粒径受喷施距离、压力的影响均在大幅减弱。同时雾滴粒径的减小确实可以提高农药的

有效沉积率。但当雾滴VMD小于190 μm时(距离喷口1 m),雾滴携带能量过低,到达果树冠层上部的雾滴有限,导致药液在冠层中部区域过多沉积并流失到地面,也会造成药液浪费。对于自走传统轴流风送喷雾机,增加的辅助气流胁迫小粒径雾滴进入冠层内部,增强雾滴在冠层的穿透性,并且扭转叶片,使得叶片近、远轴面着药,故内外膛沉积比均为0.7~0.8。

担架柱塞泵式机动喷雾机药液量流失的主要原因在于,叶片上的药液量超过最大持留量,进而导致药液滴落流失。而自走传统轴流风送喷雾机的流失途径主要是雾滴在空中的漂移。针对两种施药机械不同的药液流失途径,可采取相应的改进措施来提高其有效沉积率,对于担架柱塞泵式机动喷雾机,应在降低雾滴沉积率的同时提高液滴的初始速度为其添加辅助气流。对于自走传统轴流风送喷雾机,由于有辅助气流的帮助,雾滴粒径的大小对冠层内外沉积比影响较小,应主要增加变量喷雾技术或将自走传统轴流风送喷雾机应用于矮砧密植果园。

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